## EURAMET Project 1105

## Bilateral comparison on micro-CMM artefacts between PTB and METAS

Final report

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## 1 Introduction

In May 2009, the EURAMET contact persons for length of the Swiss Federal Office of Metrology (METAS) and of the German Physikalisch-Technische Bundesanstalt (PTB) decided to carry out a bilateral comparison for the calibration of artefacts for microcoordinate measuring machines (micro-CMM). This comparison was part of the EURAMET research collaboration project \#1105 with the title "Bilateral comparison on micro-CMM artefacts". PTB was the pilot laboratory of the comparison. Within this cooperation, comparison measurements were made on three selected test objects for micro-CMMs provided by PTB and METAS. The cooperation led to an information exchange on suitable artefacts and practical issues for handling and measurement strategies. This work will be helpful for future comparisons in the new field of microCMM calibration.

## 2 Participants

The participants and contact persons are listed in table 1.
Table 1. Participants and contact persons of the comparison.

| Laboratory <br> code | Country <br> code | Contact person, <br> laboratory | Phone, fax, email |
| :--- | :--- | :--- | :--- |
| METAS | CH | Alain Küng <br> Federal Office of Metrology <br> Lindenweg 50 <br> 3003 Bern-Wabern <br> Switzerland | Tel: +41313234641 <br> Fax:+41 31 323 32 10 |
| Alain.Kueng@metas.ch |  |  |  |

## 3 Time schedule

The original time schedule had foreseen about two months for each laboratory for the calibration, including the transportation. Due to the fragility of the Zerodur hemisphere plate and the unknown stability of the hemispheres, this plate was calibrated at PTB twice before and once after transportation to Switzerland.

Table 2. Original time schedule for the comparison measurements.

| Laboratory | Date of measurement |
| :--- | :--- |
| PTB | March 2009 |
| PTB | May 2009 |
| METAS | September 2009 |
| PTB | December 2009 |

## 4 Measurement standards

Three micro-CMM standards were circulated. Besides the already mentioned Zerodur hemisphere plate, a 1 mm calibration sphere and a 1 mm ring gauge were used. The parameters of the standards are summarized in table 3.

Table 3. Measurement standards, parameters and characteristics.

| Type | Manufacturer, <br> identification | Dimensions, <br> material | Characteristics |
| :--- | :--- | :--- | :--- |
| Hemisphere <br> plate | Zeiss IMT <br> $\# 10$ | $(90 \times 90 \times 5) \mathrm{mm}$ <br> plate: Zerodur <br> hemispheres: silicon <br> nitride, diameter 5.6 mm | 9 hemispheres with <br> irregular grid, wrung onto <br> a Zerodur plate |
| Sphere | Saphirwerk | diameter 1 mm <br> ruby <br> soldered on a tungsten <br> carbide shaft | end of shaft with a <br> kinematic mounting plate <br> to be fixed at a magnetic <br> holder |
| Ring | Cary | diameter 1 mm <br> height 0.75 mm <br> tungsten Carbide | fixed in an aluminium <br> mount |
| 1 |  |  |  |

In a first round, a 0.5 mm PTB sphere was circulated. Due to significant instabilities of its fixture, it was replaced in a second round by a 1 mm sphere provided by METAS. The 1 mm ring was found to be not suited for high-precision comparison measurements because of its large form deviations.

## 5 Measurement instructions and reporting

The participants obtained measurement instructions containing a description of the standards and instructions for handling, cleaning and transportation.

### 5.1 Zerodur hemisphere plate

The Zerodur hemisphere plate shown in figure 1 was developed and manufactured by Zeiss IMT to check micro-CMMs according to the German guideline VDI/VDE 261712.1. Nine hemispheres made of Silicon nitride, $\varnothing 5.6 \mathrm{~mm}$, are wrung onto a Zerodur plate, ( $90 \times 90 \times 5$ ) mm . The Zerodur hemisphere plate is designed especially to contact the hemispheres from both sides of the plate and, consequentially, to apply an error separation technique with up- and down-side positions of the Zerodur hemisphere plate for calibration (cf. chapter 6).

For the Zerodur hemisphere plate the xy-positions and the distances between the centre points of the hemispheres had to be calibrated in a defined object coordinate system (OCS) as shown in figure 2. The $x y$-plane of the OCS is the plane of the Zerodur plate to which the hemispheres are attached. The $x$-axis is the straight line through the centre points of the hemispheres 1 and 3 . The coordinate origin is the centre point of hemisphere $1(x y)$ and the plane of the Zerodur plate (z). The hemispheres were probed with eight points according to figure 2.


Figure 1. Zerodur plate with nine hemispheres, details: hemisphere top-side view and bottom-side view.


Figure 2. Object coordinate system and probing strategy.
The hemispheres and the Zerodur plate were cleaned with ethyl alcohol and pads using a stereo microscope for observation. The form deviations measured at the hemispheres and the Zerodur plate had to be clearly below $0.1 \mu \mathrm{~m}$, otherwise the cleaning was repeated.

### 5.2 The 1 mm Ring

For the 1 mm ring the diameter had to be calibrated at defined heights below the surface plane. The $z$-axis of the OCS is the axis of the cylinder measured with six points each at two different heights $(-0.175 \mathrm{~mm}$ and $-0.575 \mathrm{~mm})$. The $x$-axis is the perpendicular from a point in the mark " 1 " ( 2.5 mm distance to the cylinder axis) to the cylinder axis. The coordinate origin is the cylinder axis ( $x y$ ) and the surface plane of the ring $(z)$.

The diameters had to be measured at different heights $(-0.075,-0.175,-0.275,-0.375,-0.475$, -0.575 mm ) with different probing strategies ( 4 single points at $0^{\circ}, 90^{\circ}, 180^{\circ}, 270^{\circ} ; 32$ single points; 360 scanning points). No filtering was applied.


Figure 3. The 1 mm ring.

### 5.3 The 1 mm Sphere

For the 1 mm sphere different patterns were applied to sample probing points with point-to-point and scanning probing techniques. From these points the sphere diameter was determined as well as the roundness deviation in the equatorial plane. No filtering was applied. For the P1 measurement from PTB, the points were sampled according to the pattern in ISO 10360-5 and measured six times with a shift of $10^{\circ}$, resampling the coordinate system each time, before finally combining all points.

Table 4. Measurement parameters for the 1 mm sphere.

| Measurement | Element measured | Probing technique | Probing pattern | Points overall | Specifics |
| :---: | :---: | :---: | :---: | :---: | :---: |
| METAS |  |  |  |  |  |
| M1 | hemisphere $-20^{\circ} . .90^{\circ}$ | point-topoint | longitude $10^{\circ}$ latitude $5^{\circ}$ | 830 | 3-spheremethod ${ }^{[3]}$ |
| M2 | equator meridians | scanning |  | 2400 |  |
| M3 | equator | scanning |  | 1400 |  |
| PTB |  |  |  |  |  |
| P1 | hemisphere $0^{\circ} \ldots 90^{\circ}$ | point-topoint | ISO-pattern 25 points each | 150 | 6 orientations |
| P2 | hemisphere $-10^{\circ} . .90^{\circ}$ | point-topoint | longitude $10^{\circ}$ latitude $10^{\circ}$ | 256 |  |
| P3 | equator | scanning |  | 3600 |  |

## 6 Measurement instruments and methods used

METAS: Micro-coordinate measuring machine [1] using laser interferometers for length measurement; micro-probe with contact forces $<0.5 \mathrm{mN}$, probing sphere diameter 0.3 mm .

PTB: Micro-coordinate measuring machine [2] using Zerodur scales for length measurement; micro-probe with contact forces approx. 1 mN , probing sphere diameter 0.3 mm .

For the measurement of the Zerodur hemisphere plate, a reversal technique was applied to correct systematic errors of the instruments with four positions: upright position $0^{\circ}$ and $180^{\circ}$ and overturned position $0^{\circ}$ and $180^{\circ}$. At PTB, the length measurements were traced back to the SI unit the metre using parallel gauge blocks of Zerodur and quartz glass, respectively, which were calibrated with an interference comparator at PTB. Since the METAS micro-CMM uses laser interferometers which are directly traceable to the SI unit the meter, no additional length measurements were performed.

The 1 mm sphere is one of the three reference spheres from METAS. It was first calibrated in 2005 (measurement M1 in the report) using a "three sphere calibration method": a measurement of three spheres against each other to be independent of an external reference standard [3]. For the calibration of the probing sphere diameter PTB used a reference sphere which was calibrated with an interference comparator at NMi (NL).


Figure 4. Micro-CMM METAS


Figure 5. Micro-CMM PTB

## $7 \quad$ Condition and stability of the standards

PTB calibrated the Zerodur hemisphere plate twice before its transportation to METAS and once afterwards. For these calibrations the positions of the hemispheres were reproducible within $\pm 20 \mathrm{~nm}$ and, therefore, the plate was stable within the repeatability of the micro-CMM used (figure 6).


Figure 6. Zerodur hemisphere plate: positions of the hemispheres for three different calibrations at PTB - deviations from the arithmetic mean; transportation to METAS between May and December 2009, $\bullet$-position, $y$-position, $--U\left(x_{i}\right), U\left(y_{i}\right)$ for $k=2$.

The form deviations of the 1 mm ring were measured additionally at PTB with the aid of a cylinder form measuring instrument MFU110 and an optical probe. The results of these measurements are presented in appendix 4. The roundness deviations at different heights amount from $0.2 \mu \mathrm{~m}$ to $0.4 \mu \mathrm{~m}$, the straightness deviations amount from $0.2 \mu \mathrm{~m}$ to $0.8 \mu \mathrm{~m}$ and the deviations from parallelism amount from $0.4 \mu \mathrm{~m}$ to 1.0 $\mu \mathrm{m}$. During the comparison measurements different cleaning procedures were applied such as cleaning in an ultrasonic bath and mechanical cleaning using a small brush. These different cleaning procedures influenced the measurement results. Because of the large form deviations and the influence of cleaning, it was agreed that the 1 mm ring used is not suitable for high precision comparison measurements.

The 1 mm sphere has very low form deviations of less than 100 nm and could be cleaned without any difficulties. Results of roundness measurements are presented in appendix 5.

## 8 Measurement results and comparison with reference values

### 8.1 Results for the Zerodur hemisphere plate

In tables 5 and 6, all measurement results for the positions of the hemispheres within the defined coordinate system are represented together with the standard uncertainty reported (PTB: calibration in March 2009, METAS: calibration in September 2009). Due to the defined coordinate system, the coordinates $x_{1}, y_{1}$ and $y_{3}$ are zero.

Table 5. Zerodur hemisphere plate: measurement results and standard uncertainties for the $x$-coordinates of the hemispheres within the defined coordinate system.

| $\begin{array}{c}\text { Hemi- } \\ \text { sphere }\end{array}$ | $\boldsymbol{x}$ | PTB | METAS |  |
| :---: | :---: | :---: | :---: | :---: |
|  | mm | $\boldsymbol{u}(\boldsymbol{x})$ | $\boldsymbol{x}$ |  |
| nm |  |  |  |  |$)$

Table 6. Zerodur hemisphere plate: measurement results and standard uncertainties for the $y$-coordinates of the hemispheres within the defined coordinate system.

| Hemi- <br> sphere | $\boldsymbol{y}$ | PTB | METAS |  |
| :---: | :---: | :---: | :---: | :---: |
|  | mm | $\boldsymbol{u}(\boldsymbol{y})$ <br> nm | $\boldsymbol{y}$ <br> mm | $\boldsymbol{u}(\boldsymbol{y})$ <br> nm |
| 1 | 0 | 19 | 0 | 13 |
| 2 | 0.105696 | 19 | 0.105710 | 13 |
| 3 | 0 | 19 | 0 | 13 |
| 4 | 21.651562 | 20 | 21.651565 | 13 |
| 5 | 49.011533 | 22 | 49.011521 | 14 |
| 6 | 51.733546 | 22 | 51.733534 | 14 |
| 7 | 61.729616 | 24 | 61.729606 | 14 |
| 8 | 70.093179 | 25 | 70.093171 | 15 |
| 9 | 68.009434 | 24 | 68.009407 | 15 |

Figures 7 and 8 show the deviations from the weighted mean value described in chapter 9 for the coordinates of the hemispheres. The error bars represent the expanded uncertainty given by the participants ( $k=2$ ).


Figure 7. Zerodur hemisphere plate: deviations of the $x$-coordinates from the weighted mean values, $U\left(x_{i}\right)$ for $k=2$, • PTB, • METAS.


Figure 8. Zerodur hemisphere plate: deviations of the $y$-coordinates from the weighted mean values, $U\left(y_{i}\right)$ for $k=2$, ■ PTB, $\square$ METAS.

The coordinates of the hemispheres reported are compared with the reference value evaluated according to the weighted mean which takes into account the measurement uncertainty of the laboratories (cf. chapter 9). Tables 7 and 8 show the differences $\Delta x$ and $\Delta y$, respectively, of the coordinates of the hemispheres - within the defined coordinate system - to the weighted mean value and the corresponding En values. Due to the defined coordinate system, the coordinates $x_{1}, y_{1}$ and $y_{3}$ are zero and, therefore, the differences as well as the En values are zero, too.

Table 7. Zerodur hemisphere plate: differences $\Delta x$ of the $x$-coordinates with respect to the weighted mean reference value and En values.

| Hemi- <br> sphere | $\boldsymbol{\Delta} \boldsymbol{x}$ <br> nm | PTB | METAS |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  |  | $\boldsymbol{\Delta} \boldsymbol{x}$ <br> nm | En |
| 1 | 2 | 0.1 |  |  |
| 2 | 21 | 0.5 | -1 | -0.1 |
| 3 | -2 | 0.0 | -8 | -0.5 |
| 4 | 6 | 0.2 | -3 | 0.0 |
| 5 | 14 | 0.4 | -5 | -0.2 |
| 6 | 3 | 0.1 | $-\mathbf{- 1}$ | -0.4 |
| 7 | 3 | 0.1 | $-\mathbf{- 1}$ | -0.1 |
| 8 | $\mathbf{2 1}$ | $\mathbf{0 . 5}$ | $\mathbf{- 7}$ | $-\mathbf{0 . 5}$ |
|  |  |  |  | $\mathbf{0 . 5}$ |

Table 8. Zerodur hemisphere plate: differences $\Delta y$ of the $y$-coordinates with respect to the weighted mean reference value and En values.

| Hemi- <br> sphere | $\boldsymbol{\Delta y}$ <br> nm | PTB | METAS |  |
| :---: | :---: | :---: | :---: | :---: |
| $\boldsymbol{y} \boldsymbol{y}$ | En |  |  |  |
| 1 | -10 | -0.3 | 5 | 0.3 |
| 2 |  |  |  |  |
| 3 | -2 | -0.1 | 1 | 0.1 |
| 4 | 8 | 0.2 | -3 | -0.2 |
| 5 | 8 | 0.2 | -3 | -0.2 |
| 6 | 8 | 0.2 | -3 | -0.2 |
| 7 | 6 | 0.1 | -2 | -0.1 |
| 8 | $\mathbf{1 9}$ | $\mathbf{0 . 5}$ | $\mathbf{- 7}$ | $\mathbf{- 0 . 5}$ |

In table 9, results for all possible distances between the centre points of any two hemispheres are represented together with the standard uncertainty reported. The uncertainty given by METAS amounts to $U_{\mathrm{L}}($ METAS $)=33 \mathrm{~nm}+0.07 \cdot L \mathrm{~nm} / \mathrm{mm}(k=2)$ with a length dependent term. The uncertainty given by PTB amounts to $U_{\mathrm{L}}(\mathrm{PTB}) \approx$ $60 \mathrm{~nm}(k=2)$ without a length dependent term due to the negligible small length expansion coefficients of both the Zerodur hemisphere plate, the scales and the parallel gauge blocks used as length references (cf. appendix 1).

Table 9. Zerodur hemisphere plate: measurement results and standard uncertainties for the distances between the centre points of the hemispheres.

| Number | Nominal distance mm | PTB |  | METAS |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $L$ | $u(L)$ | $L$ | $u(L)$ |
|  |  | mm | nm | mm | nm |
| 1 | 12.8 | 12.810125 | 30 | 12.810126 | 17 |
| 2 | 14.7 | 14.671595 | 30 | 14.671585 | 17 |
| 3 | 18.8 | 18.823270 | 30 | 18.823259 | 17 |
| 4 | 21.7 | 21.651604 | 27 | 21.651607 | 17 |
| 5 | 24.4 | 24.395637 | 31 | 24.395637 | 17 |
| 6 | 28.2 | 28.156755 | 33 | 28.156739 | 17 |
| 7 | 32.3 | 32.283758 | 31 | 32.283757 | 18 |
| 8 | 32.9 | 32.899096 | 31 | 32.899070 | 18 |
| 9 | 36.6 | 36.592658 | 29 | 36.592639 | 18 |
| 10 | 37.8 | 37.801122 | 28 | 37.801119 | 18 |
| 11 | 39.4 | 39.429076 | 33 | 39.429050 | 18 |
| 12 | 41.9 | 41.942226 | 33 | 41.942202 | 18 |
| 13 | 43.0 | 42.985051 | 31 | 42.985039 | 18 |
| 14 | 43.5 | 43.547350 | 27 | 43.547340 | 18 |
| 15 | 46.1 | 46.092949 | 30 | 46.092934 | 18 |
| 16 | 48.4 | 48.441852 | 31 | 48.441841 | 18 |
| 17 | 49.0 | 49.029235 | 30 | 49.029209 | 18 |
| 18 | 50.7 | 50.746754 | 29 | 50.746731 | 18 |
| 19 | 51.6 | 51.635221 | 30 | 51.635194 | 18 |
| 20 | 54.7 | 54.685549 | 29 | 54.685534 | 18 |
| 21 | 60.8 | 60.844528 | 30 | 60.844512 | 19 |
| 22 | 61.9 | 61.878066 | 33 | 61.878043 | 19 |
| 23 | 63.4 | 63.441570 | 30 | 63.441547 | 19 |
| 24 | 64.6 | 64.590956 | 30 | 64.590935 | 19 |
| 25 | 65.8 | 65.779255 | 30 | 65.779244 | 19 |
| 26 | 67.5 | 67.521239 | 29 | 67.521217 | 19 |
| 27 | 68.6 | 68.608994 | 33 | 68.608967 | 19 |
| 28 | 70.1 | 70.093446 | 31 | 70.093438 | 19 |
| 29 | 70.7 | 70.699900 | 31 | 70.699871 | 19 |
| 30 | 72.0 | 71.969902 | 33 | 71.969855 | 19 |
| 31 | 74.0 | 73.981839 | 27 | 73.981810 | 19 |
| 32 | 77.2 | 77.168505 | 33 | 77.168463 | 19 |
| 33 | 78.2 | 78.180975 | 30 | 78.180952 | 19 |
| 34 | 79.6 | 79.635610 | 31 | 79.635591 | 19 |
| 35 | 91.8 | 91.792898 | 33 | 91.792860 | 20 |
| 36 | 99.7 | 99.694196 | 31 | 99.694173 | 20 |

Figure 9 shows the deviations from the weighted mean value for the distances between the centre points of the hemispheres. The error bars represent the expanded uncertainty given by the participants $(k=2)$. The length dependent deviations amount to $\Delta L / L=-0.10 \cdot 10^{-6}$ for METAS, and to $\Delta L / L=+0.25 \cdot 10^{-6}$ for PTB.


Figure 9. Zerodur hemisphere plate: deviations of the distances from the weighted mean values, $U\left(L_{i}\right)$ for $k=2, \Delta$ PTB, $\Delta$ METAS, - - least-square fit line.

The distances between the centre points of the hemispheres reported are compared with the reference value evaluated according to the weighted mean. Table 10 shows the differences $\Delta L$ of the distances to the weighted mean value and the corresponding $E n$ values.

Table 10. Zerodur hemisphere plate: differences $\Delta L$ of the distances with respect to the weighted mean reference value and En values.

| Number | Nominal distance mm | PTB |  | METAS |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\Delta L$ | En | $\Delta L$ | En |
|  |  | nm |  | nm |  |
| 1 | 12.8 | -1 | 0.0 | 0 | 0.0 |
| 2 | 14.7 | 7 | 0.1 | -2 | -0.1 |
| 3 | 18.8 | 8 | 0.2 | -3 | -0.2 |
| 4 | 21.7 | -2 | 0.0 | 1 | 0.0 |
| 5 | 24.4 | 0 | 0.0 | 0 | 0.0 |
| 6 | 28.2 | 13 | 0.2 | -3 | -0.2 |
| 7 | 32.3 | 1 | 0.0 | 0 | 0.0 |
| 8 | 32.9 | 19 | 0.4 | -6 | -0.4 |
| 9 | 36.6 | 13 | 0.3 | -5 | -0.3 |
| 10 | 37.8 | 2 | 0.0 | -1 | 0.0 |
| 11 | 39.4 | 20 | 0.3 | -6 | -0.3 |
| 12 | 41.9 | 18 | 0.3 | -5 | -0.3 |
| 13 | 43.0 | 9 | 0.2 | -3 | -0.2 |
| 14 | 43.5 | 7 | 0.2 | -3 | -0.2 |
| 15 | 46.1 | 11 | 0.2 | -4 | -0.2 |
| 16 | 48.4 | 8 | 0.2 | -3 | -0.2 |
| 17 | 49.0 | 19 | 0.4 | -7 | -0.4 |
| 18 | 50.7 | 17 | 0.3 | -7 | -0.3 |
| 19 | 51.6 | 19 | 0.4 | -7 | -0.4 |
| 20 | 54.7 | 10 | 0.2 | -4 | -0.2 |
| 21 | 60.8 | 11 | 0.2 | -4 | -0.2 |
| 22 | 61.9 | 18 | 0.3 | -6 | -0.3 |
| 23 | 63.4 | 16 | 0.3 | -6 | -0.3 |
| 24 | 64.6 | 15 | 0.3 | -6 | -0.3 |
| 25 | 65.8 | 8 | 0.2 | -3 | -0.2 |
| 26 | 67.5 | 16 | 0.3 | -7 | -0.3 |
| 27 | 68.6 | 20 | 0.4 | -7 | -0.4 |
| 28 | 70.1 | 6 | 0.1 | -2 | -0.1 |
| 29 | 70.7 | 21 | 0.4 | -8 | -0.4 |
| 30 | 72.0 | 35 | 0.6 | -12 | -0.6 |
| 31 | 74.0 | 19 | 0.4 | -10 | -0.4 |
| 32 | 77.2 | 32 | 0.5 | -10 | -0.5 |
| 33 | 78.2 | 16 | 0.3 | -7 | -0.3 |
| 34 | 79.6 | 13 | 0.3 | -5 | -0.3 |
| 35 | 91.8 | 29 | 0.5 | -10 | -0.5 |
| 36 | 99.7 | 16 | 0.3 | -7 | -0.3 |

### 8.2 Results for the 1 mm ring

In tables 11, 12 and 13, all measurement results for the diameters of the ring at different heights and for different probing strategies are represented together with the standard uncertainty reported (METAS: calibration in September 2009, PTB: calibration in February 2010).

Table 11. The 1 mm ring: measurement results and standard uncertainties for the diameters at different heights for point-to-point probing
(4 points, $0^{\circ}, 90^{\circ}, 180^{\circ}, 270^{\circ}$ ).

|  | METAS |  | PTB |  |
| :---: | :---: | :---: | :---: | :---: |
| Height | $\boldsymbol{D}$ | $\boldsymbol{u ( D )}$ | $\boldsymbol{D}$ | $\boldsymbol{u ( D )}$ |
| mm | mm | nm | mm | nm |
| points | 4 |  | 4 |  |
| -0.075 | 1.000182 | 18 | 1.000143 | 77 |
| -0.175 | 0.999598 | 18 | 0.999550 | 66 |
| -0.275 | 0.999537 | 18 | 0.999461 | 67 |
| -0.375 | 0.999707 | 18 | 0.999655 | 47 |
| -0.475 | 0.999995 | 18 | 0.999934 | 54 |
| -0.575 | 1.000555 | 18 | 1.000525 | 118 |

Table 12. The 1 mm ring: measurement results and standard uncertainties for the diameters in different heights for point-to-point probing (32 points).

|  | METAS |  | PTB |  |
| :---: | :---: | :---: | :---: | :---: |
| Height <br> mm | $\boldsymbol{D}$ <br> mm | $\boldsymbol{u}(\boldsymbol{D})$ <br> nm | $\boldsymbol{D}$ <br> mm | $\boldsymbol{u}(\boldsymbol{D})$ <br> nm |
| points | 32 |  | 32 |  |
| -0.075 | 1.000159 | 18 | 1.000263 | 28 |
| -0.175 | 0.999573 | 18 | 0.999571 | 26 |
| -0.275 | 0.999510 | 18 | 0.999495 | 26 |
| -0.375 | 0.999706 | 18 | 0.999703 | 28 |
| -0.475 | 0.999954 | 18 | 0.999946 | 28 |
| -0.575 | 1.000531 | 18 | 1.000520 | 35 |

Table 13. The 1 mm ring: measurement results and standard uncertainties for the diameters at different heights for scanning probing (382 points, 469 points).

|  | METAS |  | PTB |  |
| :---: | :---: | :---: | :---: | :---: |
| Height | $\boldsymbol{D}$ | $\boldsymbol{u ( D )}$ | $\boldsymbol{D}$ | $\boldsymbol{u}(\boldsymbol{D})$ |
| mm | mm | nm | mm | nm |
| points | 382 |  | 469 |  |
| -0.075 | 1.000090 | 18 | 1.000218 | 24 |
| -0.175 | 0.999499 | 18 | 0.999539 | 24 |
| -0.275 | 0.999418 | 18 | 0.999459 | 24 |
| -0.375 | 0.999636 | 18 | 0.999664 | 24 |
| -0.475 | 0.999877 | 18 | 0.999910 | 24 |
| -0.575 | 1.000443 | 18 | 1.000486 | 25 |

Figures 10, 11 and 12 show the deviations from the weighted mean value for the diameters of the 1 mm ring at different heights and measured with different probing strategies. The error bars represent the expanded uncertainty given by the participants ( $k=2$ ).


Figure 10. The 1 mm ring: deviations of the diameters, measured with four single points, from the weighted mean values, $U\left(D_{i}\right)$ for $k=2$, $\bullet$ PTB, $\bullet$ METAS.


Figure 11. The 1 mm ring: deviations of the diameters, measured with 32 single points, from the weighted mean values, $U\left(D_{\mathrm{i}}\right)$ for $k=2$, ■ PTB, ■ METAS.


Figure 12. The 1 mm ring: deviations of the diameters, measured with scanning, from the weighted mean values, $U\left(D_{\mathrm{i}}\right)$ for $k=2, \Delta \mathrm{PTB}, \triangle$ METAS.

The diameters of the 1 mm ring reported are compared with the reference value evaluated according to the weighted mean. Tables 14,15 and 16 show the differences $\Delta D$ of the diameters for the different probing strategies to the weighted mean value and the corresponding En values.

Table 14. The 1 mm ring: differences $\Delta D$ of the diameters measured with four single points with respect to the weighted mean reference value and En values.

|  | METAS |  | PTB |  |
| :---: | :---: | :---: | :---: | :---: |
| Height <br> mm | $\boldsymbol{\Delta \boldsymbol { D }}$ | En | $\boldsymbol{\Delta \boldsymbol { D }}$ | En |
| nm |  | nm |  |  |
| -0.075 | 4 | 4 |  |  |
| -0.175 | 2 | 0.2 | -37 | -0.2 |
| -0.275 | 5 | 0.4 | -45 | -0.4 |
| -0.375 | 6 | 0.5 | -71 | -0.5 |
| -0.475 | 6 | 0.5 | -46 | -0.5 |
| -0.575 | 1 | 0.5 | -55 | -0.5 |

Table 15. The 1 mm ring: differences $\Delta D$ of the diameters measured with 32 single points with respect to the weighted mean reference value and En values.

|  | METAS |  | PTB |  |
| :---: | :---: | :---: | :---: | :---: |
| Height <br> $m m$ | $\boldsymbol{\Delta D}$ | En | $\boldsymbol{\Delta \boldsymbol { D }}$ | En |
| points | 32 |  | 32 |  |
| -0.075 | -29 | -1.6 | $\mathbf{n m}$ | 1.6 |
| -0.175 | 1 | 0.0 | -1 | 0.0 |
| -0.275 | 5 | 0.2 | -11 | -0.2 |
| -0.375 | 1 | 0.0 | -2 | 0.0 |
| -0.475 | 2 | 0.1 | -6 | -0.1 |
| -0.575 | 2 | 0.1 | -9 | -0.1 |

Table 16. The 1 mm ring: differences $\Delta D$ of the diameters measured with scanning probing with respect to the weighted mean reference value and En values.

|  | METAS |  | PTB |  |
| :---: | :---: | :---: | :---: | :---: |
| Height | $\boldsymbol{\Delta} \boldsymbol{D}$ | $\boldsymbol{E n}$ | $\boldsymbol{\Delta} \boldsymbol{D}$ | En |
| mm | nm |  | nm |  |
| points | 382 |  | 469 |  |
| -0.075 | -45 | -2.2 | 83 | 2.2 |
| -0.175 | -14 | -0.7 | 26 | 0.7 |
| -0.275 | -15 | -0.7 | 27 | 0.7 |
| -0.375 | -10 | -0.5 | 18 | 0.5 |
| -0.475 | -12 | -0.6 | 21 | 0.6 |
| -0.575 | -14 | -0.7 | 28 | 0.7 |

### 8.3 Results for the $1 \mathbf{m m}$ sphere

In table 17, all measurement results for the diameters of the sphere measured with different probing strategies are represented together with the standard uncertainty reported (METAS: calibration in September 2009, PTB: calibration in February 2010).

Table 17. The 1 mm sphere: measurement results and standard uncertainties of the diameters measured with different probing strategies.

| Measure- <br> ment | Element <br> measured | Probing <br> technique | Points <br> overall | $\boldsymbol{D}$ <br> mm | $\boldsymbol{u ( D )}$ <br> nm |
| :---: | :---: | :---: | :---: | :---: | :---: |
| METAS |  |  |  |  |  |
| M1 | hemisphere, $-20^{\circ} \ldots 90^{\circ}$ | point-to-point | 828 | 1.000824 | 18 |
| M2 | equator, meridians | scanning | 2326 | 1.000838 | 18 |
| M3 | equator | scanning | 1358 | 1.000838 | 18 |
| PTB |  |  |  |  |  |
| P1 | hemisphere, $0^{\circ} \ldots 90^{\circ}$ | point-to-point | 150 | 1.000777 | 25 |
| P2 | hemisphere, $-10^{\circ} . .90^{\circ}$ | point-to-point | 256 | 1.000803 | 25 |
| P3 | equator | scanning | 3600 | 1.000789 | 23 |

Figure 13 shows the deviations from the weighted mean value for the diameters of the 1 mm sphere measured with different probing strategies. The error bars represent the expanded uncertainty given by the participants $(k=2)$.


Figure 13. The 1 mm sphere: deviations of the diameters, measured with different probing strategies, from the weighted mean values, $U\left(D_{\mathrm{i}}\right)$ for $k=2$, • PTB, • METAS (for symbols Mi and Pi cf. chapter 5.3, too).

The diameters at the 1 mm sphere reported are compared with the reference value evaluated according to the weighted mean. Table 18 shows the differences $\Delta D$ of the diameters for the different probing strategies to the weighted mean value and the corresponding En values.

Table 18. The 1 mm sphere: differences $\Delta D$ of the diameters measured with different probing strategies with respect to the weighted mean reference value and En values.

| Measure- <br> ment | Element <br> measured | Probing <br> technique | Points <br> overall | $\Delta \boldsymbol{D}$ <br> nm | En |
| :---: | :---: | :---: | :---: | :---: | :---: |
| METAS |  |  |  |  |  |
| M1 | hemisphere, $-20^{\circ} \ldots 90^{\circ}$ | point-to-point | 828 | 6 | 0.2 |
| M2 | equator, meridians | scanning | 2326 | 20 | 0.6 |
| M3 | equator | scanning | 1358 | 20 | 0.6 |
| PTB |  |  |  |  |  |
| P1 | hemisphere, $0^{\circ} \ldots 90^{\circ}$ | point-to-point | 150 | -41 | -0.9 |
| P2 | hemisphere, $-10^{\circ} . .90^{\circ}$ | point-to-point | 256 | -15 | -0.3 |
| P3 | equator | scanning | 3600 | -29 | -0.7 |

## 9 Evaluation of the measurement results

In the course of the comparison measurements, complete measurement results $X_{i}=x_{i} \pm u\left(x_{i}\right)$ were obtained independently for the same physical quantity $Y$ at the laboratories, using different measurement devices. The measurement results obtained are fitted on the assumption that the measurands $X_{i}$ are identical with $Y$.

The reference value is calculated by the weighted mean as follows:

$$
\begin{equation*}
y=\sum_{i=1}^{n} g_{i} x_{i} \tag{1}
\end{equation*}
$$

with

$$
\begin{equation*}
g_{i}=u^{2}(y) / u^{2}\left(x_{i}\right) \tag{2}
\end{equation*}
$$

and

$$
\begin{equation*}
u^{2}(y)=\left[\sum_{i=1}^{n} 1 / u^{2}\left(x_{i}\right)\right]^{-1} . \tag{3}
\end{equation*}
$$

According to eq. (3), the uncertainty of the weighted mean $u(y)$ is influenced only by the uncertainties $u\left(x_{i}\right)$ and not by the dispersion of the values measured. The best estimate of the difference between the measured value and the reference value is $\Delta x_{i}=x_{i}-y$, and the associated standard uncertainty according to GUM is:

$$
\begin{equation*}
u\left(\Delta x_{i}\right)=\left[u^{2}\left(x_{i}\right)+u^{2}(y)-2 u\left(x_{i}, y\right)\right]^{1 / 2} . \tag{4}
\end{equation*}
$$

As $y$ is calculated according to eq. (1), $y$ and $x_{i}$ are correlated and the following is valid:

$$
\begin{equation*}
u\left(x_{i}, y\right)=u^{2}(y) . \tag{5}
\end{equation*}
$$

From this it follows for the standard uncertainty of the difference between the measured value and the reference value:

$$
\begin{equation*}
u\left(\Delta x_{i}\right)=\left[u^{2}\left(x_{i}\right)-u^{2}(y)\right]^{1 / 2} \tag{6}
\end{equation*}
$$

The En value is calculated by

$$
\begin{equation*}
E n=\Delta x_{i} / 2 u\left(\Delta x_{i}\right) . \tag{7}
\end{equation*}
$$

## 10 Measurement uncertainty

The measurement uncertainty and the uncertainty budgets were evaluated in accordance to the ISO Guide to the expression of uncertainty in measurement (GUM). The uncertainty budgets of PTB and METAS for the different measurands are presented in appendices 1 to 3 .

## 11 Conclusions

This measurement comparison of micro-CMM artefacts was of great benefit for the participants. It was the first comparison within EURAMET in the field of microcoordinate measurement techniques. Moreover, the Zerodur hemisphere plate is a newly developed standard to check micro-CMMs at a high-precision level and no profound experience has existed up to now for comparison with uncertainties in the range of about 50 nm .

The results obtained at both laboratories agree within the small uncertainties which are clearly below 100 nm , with the exception of a few measurements at the 1 mm ring definitely due to its large form deviations. This very good agreement highlights the state of the art of the very precise micro-CMMs used and, moreover, the advanced practice of calibration work of micro-CMM artefacts at METAS and PTB.

It has been shown, that the Zerodur hemisphere plate is stable within a few nm and suited for comparison of micro-CMM measurements with very low uncertainty. The comparison showed furthermore, that the standards may have a significant influence on the uncertainty and, therefore, the comparability of measurement results. The relative large form deviations of the 1 mm ring strongly influenced the measurement uncertainty and did not allow a comparability of measurements with high precision. This was no issue for the measurement at the 1 mm sphere because of its very low form deviations. The initially proposed 0.5 mm sphere exhibited a time-dependent bending, probably due to creep of the glue between the sphere and the shaft once stressed by the contact forces. The stability of the fragile Zerodur hemisphere plate could be ensured by appropriate handling, cleaning and transportation.

## References

[1] Küng A, Meli F, Thalmann R: Ultraprecision micro-CMM using a low force 3D touch probe. 2007 Meas. Sci. Technol. 18 319-327
[2] http://www.zeiss.de/f25
[3] Küng A, Meli F: Self calibration method for 3D roundness of spheres using an ultraprecision coordinate measuring machine. Proc. of 5th euspen International Conference, Montpellier, France, May 2005, Volume1, p. 193
[4] Krystek M, Anton M: A weighted total least-squares algorithm for fitting a straight line. 2007 Meas. Sci. Technol. 18 3438-3442

## Appendix 1: Uncertainty budgets for the Zerodur hemisphere plate

At PTB the uncertainty of positions of hemispheres and the respective distances were estimated using the GUM-Workbench software. Tables 19a and 19b show the uncertainty budget for the positions.

Table 19a. Zerodur hemisphere plate: uncertainty budget of PTB for the positions of hemispheres (part 1)

| Quantity | Symbol | Unit | $\boldsymbol{x}_{i}$ | $\pm \Delta \boldsymbol{x}_{i}$ | $u\left(x_{i}\right)$ | Distrib. | $c_{i}$ | $u_{i}(\boldsymbol{y})$ | Index \% |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $x$-Position centre point (mean) | $\chi_{M}$ | mm | 71.5 |  | 3.0E-06 |  |  |  |  |
| Correction of scale factor | $K$ | mm | -1.3E-07 |  | 2.2E-07 |  |  |  |  |
| Sum of correction values | $\Delta X$ | mm | 2.0E-07 |  | 1.8E-05 |  |  |  |  |
| $x$-Position centre point (orientation 1) | $X_{1}$ | mm | 70.6998724 |  | 7.0E-06 | normal | 0.25 | 1.7E-06 | 1 |
| $x$-Position centre point (orientation 2) | $X_{2}$ | mm | 70.6998986 |  | 7.0E-06 | normal | 0.25 | 1.7E-06 | 1 |
| $x$-Position centre point (orientation 3) | $X_{3}$ | mm | 70.6998739 |  | 7.0E-06 | normal | 0.25 | 1.7E-06 | 1 |
| $x$-Position centre point (orientation 4) | $X_{4}$ | mm | 70.6998942 |  | 7.0E-06 | normal | 0.25 | 1.7E-06 | 1 |
| Deviation parallel gauge block 1 (long) | $\delta X_{1}$ | mm | -4.0E-06 |  | 1.1E-05 |  |  |  |  |
| Deviation parallel gauge block 2 (short) | $\delta X_{2}$ | mm | -1.3E-05 |  | 1.1E-05 |  |  |  |  |
| Reference length gauge block 1 | $X_{1 R}$ | mm | 80.153481 |  | $1.0 \mathrm{E}-05$ | normal | 1 | 1.0E-05 | 17 |
| Reference length gauge block 2 | $X_{2 R}$ | mm | 9.499996 |  | 1.0E-05 | normal | -1 | -1.0E-05 | 17 |
| Indicated length gauge block 1 | $X{ }_{1 M}$ | mm | 80.153477 |  | $5.0 \mathrm{E}-06$ | normal | -1 | -5.1E-06 | 4 |
| Indicated length gauge block 2 | $X_{2 M}$ | mm | 9.499983 |  | 5.0E-06 | normal | 1 | 5.1E-06 | 4 |
| Uncorrected systematic deviations micro-CMM | $\Delta X_{0}$ | mm | 0 | $2.0 \mathrm{E}-05$ | 1.2E-05 | rectang. | 1 | 1.2E-05 | 22 |
| Temperature influence meas. gauge block 1 | $\Delta X_{1}$ | mm | 0 |  | 1.2E-06 |  |  |  |  |
| Temperature influence meas. gauge block 2 | $\Delta X_{2}$ | mm | 2.4E-07 |  | 2.7E-07 |  |  |  |  |
| Flatness, roughness gauge block 1 | $\Delta X_{3}$ | mm | 0 | 1.0E-06 | 5.8E-07 | rectang. | 1 | 5.8E-07 | 0 |
| Flatness, roughness gauge block 2 | $\Delta X_{4}$ | mm | 0 | 1.0E-06 | $5.8 \mathrm{E}-07$ | rectang. | 1 | 5.8E-07 | 0 |
| Thermal drift during measurement | $\Delta X_{5}$ | mm | 0 | 1.0E-05 | 5.8E-06 | rectang. | 1 | 5.8E-06 | 6 |
| Temperature influence Zerodur plate | $\Delta X_{6}$ | mm | 0 |  | 2.1E-07 |  |  |  |  |

Table 19b. Zerodur hemisphere plate: uncertainty budget of PTB for the positions of hemispheres (part 2),
OCS, object coordinate system.

| Quantity | Symbol | Unit | $\boldsymbol{x}_{\boldsymbol{i}}$ | $\pm \Delta \boldsymbol{x}_{i}$ | $u\left(x_{i}\right)$ | Distrib. | $c_{i}$ | $u_{i}(\boldsymbol{y})$ | $\begin{gathered} \text { Index } \\ \% \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Form deviations hemispheres, probing sphere | $\Delta X_{7}$ | mm | 0 | 1.0E-05 | 5.8E-06 | rectang. | 1 | $5.8 \mathrm{E}-06$ | 6 |
| Temperature influence scales | $\Delta X_{8}$ | mm | 0 |  | 2.1E-07 |  |  |  |  |
| Calibration of OCS at Zerodur hemisphere plate | $\Delta X_{9}$ | mm | 0 | 1.0E-05 | 5.8E-06 | rectang. | 1 | 5.8E-06 | 6 |
| Calibration of OCS at gauge block 1 | $\Delta X_{10}$ | mm | 0 | 5.0E-06 | 2.9E-06 | rectang. | 1 | 2.9E-06 | 1 |
| Calibration of OCS at gauge block 2 | $\Delta X_{11}$ | mm | 0 | 2.0E-06 | 1.2E-06 | rectang. | 1 | $1.2 \mathrm{E}-06$ | 0 |
| Angle deviations gauge blocks to scales | $\Delta X_{12}$ | mm | 0 | 5.0E-06 | 2.9E-06 | rectang. | 1 | 2.9E-06 | 1 |
| Variation scale correction factor | $\Delta K$ | mm | 0 |  | 9.00E-06 | normal | 1 | 9.0E-06 | 13 |
| Thermal expansion coefficient gauge block 1 | $\alpha_{1}$ | 1/K | 0 | 5.0E-07 | 2.9E-07 | rectang. | 4 | $1.2 \mathrm{E}-06$ | 0 |
| Temperature deviation gauge block 1 | $\Delta T_{1}$ | K | 0.05 |  | 0.05 | normal | 0 | 0 | 0 |
| Thermal expansion coefficient gauge block 2 | $\alpha_{2}$ | 1/K | $5.0 \mathrm{E}-07$ | 5.0E-07 | $2.9 \mathrm{E}-07$ | rectang. | 0.47 | $1.4 \mathrm{E}-07$ | 0 |
| Temperature deviation gauge block 2 | $\Delta T_{2}$ | K | 0.05 |  | 0.05 | normal | 4.7E-06 | $2.4 \mathrm{E}-07$ | 0 |
| Thermal expansion coefficient Zerodur plate | $\alpha_{3}$ | 1/K | 0 | 1.0E-07 | $5.8 \mathrm{E}-08$ | rectang. | 3.6 | 2.1E-07 | 0 |
| Temperature deviation Zerodur plate | $\Delta T_{3}$ | K | 0.05 |  | 0.05 | normal | 0 | 0 | 0 |
| Thermal expansion coefficient scales | $\alpha_{4}$ | 1/K | 0 | 1.0E-07 | 5.8E-08 | rectang. | 3.6 | $2.1 \mathrm{E}-07$ | 0 |
| Temperature deviation scales | $\Delta T_{4}$ | K | 0.05 |  | 0.05 | normal | 0 | 0 | 0 |
| $x$-Position centre point | $X$ | mm | 70.699876 |  |  |  |  |  |  |
| Standard uncertainty | $u(X)$ | mm |  |  |  |  |  | 0.000025 |  |
| Coverage factor |  |  |  |  |  |  |  | 2 |  |
| Expanded uncertainty | $U(X)$ | mm |  |  |  |  |  | 0.000050 |  |

Table 20 shows the uncertainty budget of PTB for the distance between hemispheres 3 and 8 as an example.
Table 20. Zerodur hemisphere plate: uncertainty budget of PTB for the distance between hemispheres 3 and 8 as an example.

| Quantity | Symbol | Unit | $\boldsymbol{x}_{\boldsymbol{i}}$ | $u\left(x_{i}\right)$ | Distrib. | $c_{i}$ | $u_{i}(y)$ | Index \% |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $x$-Position hemisphere 3 | $x_{3}$ | mm | 70.699900 | 2.5E-05 | normal | 0.71 | 1.8E-05 | 39 |
| $y$-Position hemisphere 3 | $y_{3}$ | mm | 0 | 1.9E-05 | normal | -0.71 | $1.3 \mathrm{E}-05$ | 11 |
| $x$-Position hemisphere 8 | $x_{8}$ | mm | -0.193534 | 1.9E-05 | normal | -0.71 | 1.3E-05 | 11 |
| $y$-Position hemisphere 8 | $y_{8}$ | mm | 70.093179 | 2.5E-05 | normal | 0.71 | $1.8 \mathrm{E}-05$ | 39 |
| Distance | $L$ | mm | 99.694196 |  |  |  |  |  |
| Standard uncertainty | $u(L)$ | mm |  |  |  |  | 0.000031 |  |
| Coverage factor |  |  |  |  |  |  | 2 |  |
| Expanded uncertainty | $U(L)$ | mm |  |  |  |  | 0.000062 |  |

Tables 21a and 21 b show the uncertainty budget of METAS for the measurement of the Zerodur hemisphere plate.
Table 21a. Zerodur hemisphere plate: uncertainty budget of METAS for each of the coordinate of the hemispheres.


Quadratic form: $Q[25,0.23 \mathrm{~L}]$

| $U\left(L=L_{\text {min }}\right)=$ | 25 nm |
| :--- | :--- |
| $U\left(L=L_{\text {max }}\right)=$ | 29 nm |

Table 21b. Zerodur hemisphere plate: uncertainty budget of METAS for the distances of hemispheres.


## Appendix 2: Uncertainty budgets for the $1 \mathbf{m m}$ ring

Table 22 shows the uncertainty budget of PTB for the measurement of the 1 mm ring. The influence of the form deviations on the evaluation of the diameter $\Delta A i$ by least-square fitting was estimated with a method developed by Krystek and Anton [4].

Table 22. The 1 mm ring: uncertainty budget of PTB for diameter measurement at a height -0.075 mm as an example.

| Quantity $X_{i}$ probing strategy | Symbol | Unit | $\boldsymbol{x}_{i}$ | $\pm \Delta \boldsymbol{X}_{i}$ | $u\left(x_{i}\right)$ | Distrib. | $c_{i}$ | $v i$ | 4EP | $\begin{aligned} & u_{i}(\boldsymbol{y}) \\ & 32 E P \end{aligned}$ | SC |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Diameter ring | D | mm | 1 |  |  |  | 4.5E-07 | 100 | 0.5 | 0.5 | 0.5 |
| Temperature deviation | $\Delta t$ | K | 0.05 |  |  | rectang. |  |  |  |  |  |
| Uncertainty of temperature meas. | $u(t)$ | K |  |  | 0.1 | normal |  |  |  |  |  |
| Thermal expansion coefficient | $\alpha$ | $\mathrm{K}^{-1}$ | 4.5E-06 |  |  |  |  |  |  |  |  |
| Uncertainty of thermal exp. coeff. | $u(\alpha)$ | $\mathrm{K}^{-1}$ |  |  | 4.5E-07 | rectang. |  |  |  |  |  |
| Standard deviation ( $n=20$ ) | $s$ | nm |  |  | 8 | normal | 1 | 19 | 2 | 2 | 3 |
| Drift after measurement | $\Delta P$ | nm | 0 | 5 | 3 | rectang. | 1 | 100 | 3 | 3 | 3 |
| Diameter reference sphere | $d r$ | nm | 0 |  | 20 | normal | 1 | 100 | - 20 | 20 | 20 |
| Form deviations reference sphere | $\Delta F d r$ | nm | 0 | 5 | 3 | rectang. | 1 | 100 | 3 | 3 | 3 |
| Standard dev. calibration probing sphere | $s d t$ | nm |  |  | 6 | normal | 1 | 9 | 6 | 6 | 6 |
| Form deviation probing sphere | $\Delta F d t$ | nm | 0 | 10 | 6 | rectang. | 1 | 100 | 6 | 6 | 6 |
| Systematic deviations F25 | $\triangle C A A$ | nm | 0 | 10 | 6 | rectang. | 1 | 100 | 6 | 6 | 6 |
| Influence form dev. on evaluation diameter | $\Delta A$ | nm | 0 |  |  | normal | 1 | 100 | 64 | 15 | 4 |
| Influence form dev. for angle variation | $\Delta W$ | nm | 0 | 60 | 35 | rectang. | 1 | 100 | 35 |  |  |
| Influence form dev. for variation of height | $\Delta H$ | nm | 0 | 10 | 6 | rectang. | 1 | 100 | 6 | 6 | 6 |
| Cleaning | $\Delta R e$ | nm | 0 | 5 | 3 | rectang. | 1 | 100 | 3 | 3 | 3 |
| Definition object coordinate system | $\Delta$ def | nm | 0 | 5 | 3 | rectang. | 1 | 100 | 3 | 3 | 3 |
| Standard uncertainty | $u(D)$ | nm |  |  |  | normal |  |  | 77 | 28 | 24 |
| Degrees of freedom | $v_{\text {eff }}$ |  |  |  |  |  |  |  | 187 | 277 | 194 |
| Coverage factor | $k$ |  |  |  |  |  |  |  | 2 | 2 | 2 |
| Expanded uncertainty | $\boldsymbol{U}(\mathrm{D})$ | nm |  |  |  |  |  |  | 154 | 56 | 49 |

Table 23 shows the uncertainty budget of METAS for the measurement of the 1 mm ring.
Table 23. The 1 mm ring: uncertainty budget of METAS for diameter measurements.


| Quadratic form: $\mathrm{Q}[35,0.32 \mathrm{~L}]$ |  |
| :---: | :---: |
| $\mathrm{U}\left(\mathrm{L}=L_{\text {min }}\right)=$ | 35 nm |
| $\mathrm{U}\left(\mathrm{L}=L_{\text {max }}\right)=$ | 35 nm |
| Linearized form: $35+0.00 \mathrm{~L} \mathrm{~nm}$ |  |

## Appendix 3: Uncertainty budgets for the 1 mm sphere

Table 24 shows the uncertainty budget of PTB for the measurement of the 1 mm sphere. The influence of the form deviations on the evaluation of the diameter $\Delta A$ by least-square fitting was estimated with a method developed by Krystek and Anton [4].

Table 24. The 1 mm sphere: uncertainty budget of PTB for diameter measurements.

| Quantity $\boldsymbol{X}_{\boldsymbol{i}}$ <br> Measurement strategy | Symbol | Unit | $\boldsymbol{x}_{i}$ | $\pm \Delta \boldsymbol{x}_{\boldsymbol{i}}$ | $u\left(x_{i}\right)$ | Distrib. | $c_{i}$ | $v i$ | $u_{i}(\boldsymbol{y})$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  | Sphere | Equator |
| Diameter (in mm) | D | mm | 1 |  |  |  | 5.4E-07 | 100 | 0.5 | 0.5 |
| Temperature deviation | $\Delta t$ | K | 0.05 |  |  | rectang. |  |  |  |  |
| Uncertainty of temperature meas. | $u(t)$ | K |  |  | 0.1 | normal |  |  |  |  |
| Thermal expansion coefficient | $\alpha$ | $\mathrm{K}^{-1}$ | 5.4E-06 |  |  |  |  |  |  |  |
| Uncertainty of thermal exp. coeff. | $u(\alpha)$ | $\mathrm{K}^{-1}$ |  |  | 5.4E-07 | rectang. |  |  |  |  |
|  | $s$ | $n m$ |  |  | 5 | normal | 1 | 9 | 1.6 |  |
| Standard deviation | $s$ | nm |  |  | 15 | normal | 1 | 9 |  | 5 |
| Drift after measurement | $\Delta P$ | nm | 0 | 10 | 10 | rectang. | 1 | 100 | 3 | 3 |
| Diameter reference sphere | $d r$ | nm | 0 |  | 20 | normal | 1 | 100 | 20 | F 20 |
| Form deviations reference sphere | $\Delta F d r$ | nm | 0 | 10 | 10 | rectang. | 1 | 100 | 3 | 3 |
| Standard dev. calibration probing sphere | $s d t$ | nm |  |  | 11 | normal | 1 | 9 | 3 | 3 |
| Form deviation probing sphere | $\Delta F d t$ | nm | 0 | 20 | 20 | rectang. | 1 | 100 | 6 | 6 |
| Systematic deviations F25 | $\triangle C A A$ | nm | 0 | 20 | 6 | rectang. | 1 | 100 | 6 | 6 |
| Influence form dev. on evaluation diameter | $\triangle A$ | nm | 0 |  |  | normal | 1 | 100 | 2 | 9 |
| Influence form dev. for variation of height | $\Delta H$ | nm | 0 | 10 | 3 | rectang. | 1 | 100 |  | 3 |
| Cleaning | $\Delta R e$ | nm | 0 | 5 | 1 | rectang. | 1 | 100 | 1 | 1 |
| Definition object coordinate system | $\Delta$ def | nm | 0 |  | 1 | rectang. | 1 | 100 | 1 | 1 |
| Standard uncertainty | $u(D)$ | nm |  |  |  | normal |  |  | 23 | 25 |
| Degrees of freedom | $v_{\text {eff }}$ |  |  |  |  |  |  |  | 157 | 213 |
| Coverage factor | $k$ |  |  |  |  |  |  |  | 2 | 2 |
| Expanded uncertainty | $U(D)$ | nm |  |  |  |  |  |  | 45 | 50 |

Table 25 shows the uncertainty budget of METAS for the diameter measurement at the 1 mm sphere.
Table 25. The 1 mm sphere: Uncertainty budget of METAS for diameter measurements.

| Measurement task: <br> Parameter: <br> Description: | Sapphire Sphere di L min $L$ max $\alpha$ | sphere $\varnothing=1 \mathrm{~mm}$ meter <br> 0 mm <br> 1 mm <br> $4.5 \mathrm{ppm} /{ }^{\circ}$ | rom METAS $L_{\text {spez }}$ | 1 mm |  | const. prop. $L$ std.uns./nm |  | for $L_{\text {spec }}$. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | variable | uns. [unit] | distribution | $v$ | sensitivity coefficient |  |  |  |
| Temperature difference | $\Delta \mathrm{t}$ | $0.025{ }^{\circ} \mathrm{C}$ | 1 | 100 | $4.50 \mathrm{E}+00 \mathrm{~L} \mathrm{~nm} /{ }^{\circ} \mathrm{C}$ |  | 0.113 | 0.1 |
| Uncertainty on the temperature difference | 8t | $0.002{ }^{\circ} \mathrm{C}$ | 1 | 100 | $4.50 \mathrm{E}+00 \mathrm{~L} \mathrm{~nm} /{ }^{\circ} \mathrm{C}$ |  | 0.009 | 0.0 |
| Uncertainty on the expansion coefficient | $\Delta \alpha$ | $5.0 \mathrm{E}-07^{\circ} \mathrm{C}^{-1}$ | 1.73 | 100 | $2.5 \mathrm{E}+04 \mathrm{Lnm}{ }^{* \circ} \mathrm{C}$ |  | 0.007 | 0.0 |
| Coordinate system misalignment | $\phi$ | 5.0E-05 rad | 1 | 100 | 2.5E-05 L |  | 0.001 | 0.0 |
| Reference sphere diameter | D | 15 nm | 1 | 100 | 1 | 15.0 |  | 15.0 |
| Repeatability of the probe diameter calibration | Kd | 2 nm | 1.73 | 100 | 1 | 1.2 |  | 1.2 |
| Repeatability of the probe form calibration | Kf | 0 nm | 1.73 | 100 | 1 | 0.0 |  | 0.0 |
| Residual formerror of the machine mirrors | $\Delta \mathrm{M}$ | 10 nm | 1.73 | 100 | 1 | 5.8 |  | 5.8 |
| Probing repeatability in 1 point | ¢p | 4 nm | 1 | 100 | 1 | 3.5 |  | 3.5 |
| Length dependent error of the machine | $\delta \mathrm{L}$ | 0.2 ppm | 1.73 | 100 | 1 |  | 0.116 | 0.1 |
| Drift | D | 10 nm | 1.73 | 100 | 1 | 5.8 |  | 5.8 |
|  |  |  |  |  | Standard uncertainty | 17.5 | 0.162 | 17.5 |
|  |  |  |  |  | $v_{\text {eff }}$ | 176 | 202 | 176 |
|  |  |  |  |  | k 95\% | 1.974 | 1.972 | 1.974 |
|  |  |  |  |  | ended uncertainty ( $\mathrm{U}_{95}$ ) | 35 | 0.3 | 35 |


| Quadratic form: $\mathrm{Q}[35,0.32 \mathrm{~L}]$ |  |
| :---: | :---: |
| $\mathrm{U}\left(\mathrm{L}=L_{\text {min }}\right)=$ | 35 nm |
| $\mathrm{U}\left(\mathrm{L}=L_{\text {max }}\right)=$ | 35 nm |
| Linearized form: $35+0.00 \mathrm{~L} \mathrm{~nm}$ |  |

## Appendix 4: Form measurement results at the 1 mm ring

Form measurements were not part of the comparison measurements but the form deviations should be considered for the evaluation of the uncertainty of the diameter measurements. Table 25 summarizes the roundness deviations obtained by measurements with the F25 at PTB. Additionally, for better visualization, the ring was measured at PTB with a cylinder form measuring instrument MF110 and an optical sensor. The form deviations obtained are shown in figure 14.

Table 25. The 1 mm ring: roundness deviations measured with F25 and different numbers of points (4 and 32 points, point-to-point probing, 382 points, scanning probing).

| Height <br> mm | RON $\boldsymbol{t}$ <br> $\mu \mathrm{m}$ |  |  |
| :---: | :---: | :---: | :---: |
| points | 0.13 | 32 | 382 |
| -0.075 | 0.10 | 0.26 | 0.32 |
| -0.175 | 0.11 | 0.15 | 0.15 |
| -0.275 | 0.05 | 0.19 | 0.19 |
| -0.375 | 0.06 | 0.23 | 0.30 |
| -0.475 |  | 0.24 | 0.32 |



Figure 14. The 1 mm ring: form deviations measured with MFU110, roundness deviations shown near the upper end of the cylinder, straightness deviations at $90^{\circ}$ and $270^{\circ}$. No filtering was applied.

## Appendix 5: Form measurement results at the 1 mm sphere

Figure 15 and figure 16 show form measurement results obtained with the METAS micro-CMM and the PTB-micro CMM, resp. The measurements are carried out in scanning mode. The form deviation of the hemisphere amounts to about 100 nm . The form deviation at the equatorial zone amounts to about 60 nm (unfiltered) and 30 nm (filtered), resp. Note: the form deviations of the probing sphere used is included in the results.


Figure 15. Form deviations of the 1 mm sphere measured with the METAS micro-CMM using scanning back and forth at the equator and the two polar half meridians, number of points 2326, unfiltered, form deviations 103 nm .


Figure 16. Roundness deviations of the 1 mm sphere measured at the equator with the PTB micro-CMM in scanning mode, number of points 3745, outer profile unfiltered: RON $t=60 \mathrm{~nm}$, inner profile filtered with Gauß filter, $150 \mathrm{rpm}: \operatorname{RON} t=31 \mathrm{~nm}$.

